

EXTENDED KALMAN FILTERING APPLIED TO THE POSI-
TION LOCATING AND REPORTING SYSTEM (PLRS)

Bernard M. de Mahy

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THESIS

EXTENDED KALMAN FILTERING APPLIED TO THE POSITION
LOCATING AND REPORTING SYSTEM (PLRS)

by

Bernard M. de Mahy, Jr.

December 1976

Thesis Advisor:

H. A. Titus

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AND REPORTING SYSTEM (PLRS)

by

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Captain, United States Marine Corps
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requirements for the degree of

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ABSTRACT

The Marine Corps and Army are developing a Position Locating Reporting System to aid the battlefield commander in locating his assets during battle.

This study has applied Extended Kalman Filtering techniques to that problem, evolving from a simple Extended Kalman Filter Observer to three moving observers, whose position is uncertain, estimating the position of another unit.

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I. INTRODUCTION

The precise location of all assets in and about the battle area is of prime importance to the tactical Marine Commander. In the past locating has had to depend on the individual knowing his own position and being able to report it through radio links to higher command. This system suffered from the limitations of terrain, daylight, weather, and the volume of radio traffic during battle.

To alleviate these shortcomings the Marine Corps and Army are investigating a Position Locating and Reporting System (PLRS) to collect, process, and, display the location of units, vehicles, and aircraft in and about the battle area.

The PLRS consists of field units and a master unit. The field unit is compact enough to be carried in the field by a man, vehicle, or aircraft. These units will determine the range to other field units in the area and report this information to the master unit for processing and display. The range information is determined by measuring the time required to send a signal from one unit to another and back again plus some "system" delay. When a unit's position is being updated it is referred to as the "Update" unit; and all others are referred to as "Ranging" units.

In a previous study in this area,[1], tests were conducted to investigate the use of the error ellipse in visually displaying the degree of uncertainty of the position of an update unit and the effect of numerous updates on reducing that degree of uncertainty. It was

found that the degree of uncertainty is reduced in the direction of the ranging unit with consecutive updates as shown in Fig 1 taken from that study.

That study also simulated one jet aircraft flying Mach 1 in a constant radius turn as an update unit being ranged on by two stationary ranging units to explore the proper random forcing excitation covariance necessary for adequate filter performance.

It is the intent of this study to further expand the simulation begun in the previous work by adding an additional ranging unit, allowing the movement of the ranging units, and considering the effect of ranging from a unit whose position is not known exactly

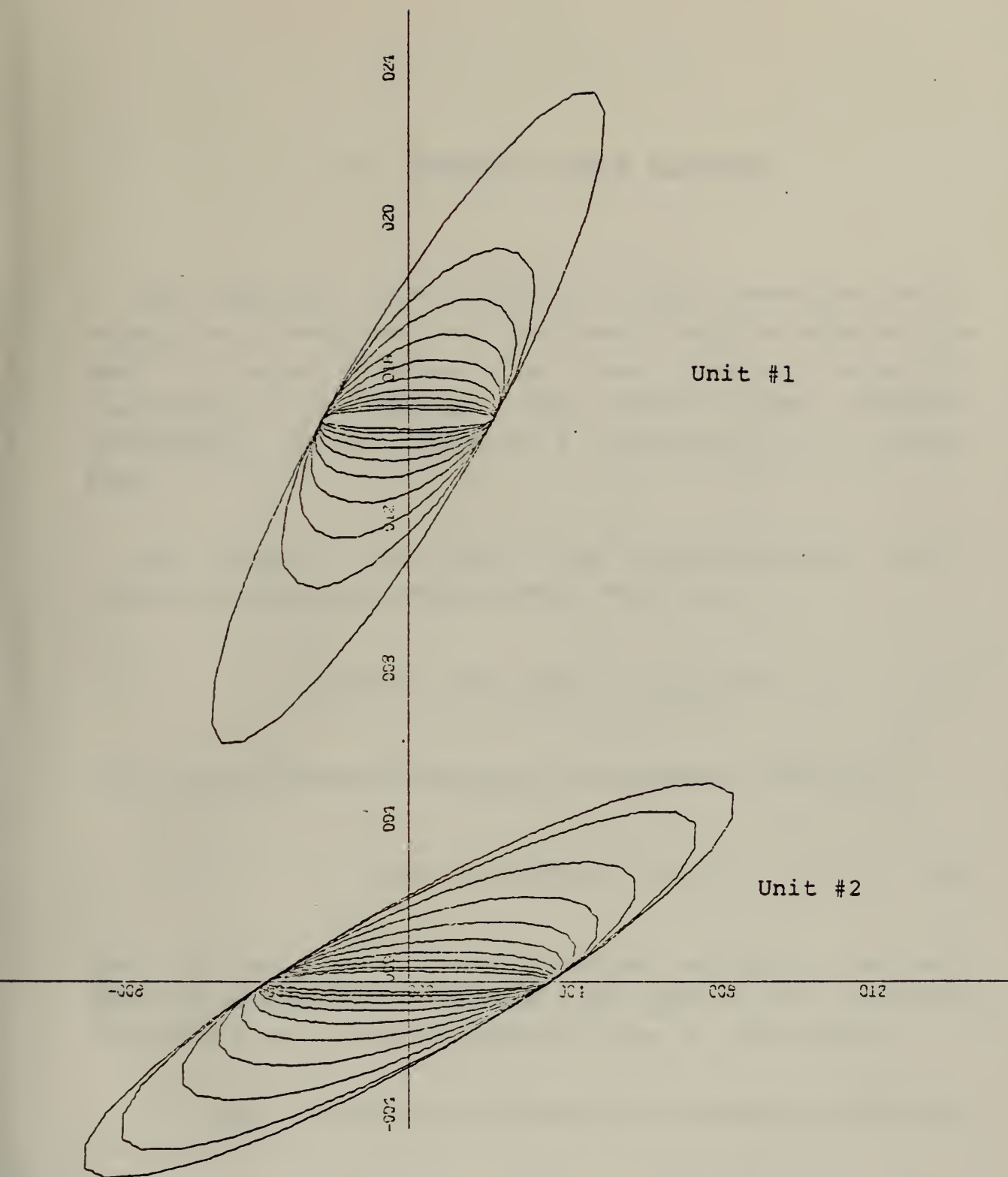


Figure 1 - CONSECUTIVE UPDATES WILL REDUCE THE DEGREE OF
UNCERTAINTY IN THE DIRECTION OF THE RANGING UNIT

II. EXTENDED KALMAN FILTERING

The Extended Kalman Filter is widely documented and no attempt at a development of that theory will be made in this work. A brief treatment has been included to establish nomenclature and formulas used. For a more complete development one is referred to reference [2] or similar texts.

As defined in this work, PLRS is described by a set of discrete, linear, cartesian system equations

$$\underline{x}(k+1) = \underline{\phi}(k) \underline{x}(k) + \underline{\Gamma}(k) \underline{w}(k) \quad (1)$$

and a set of discrete non-linear measurement equations

$$\underline{z}(k) = \underline{m}(\underline{x}(k), k) + \underline{v}(k) \quad (2)$$

where $\underline{\phi}$ and $\underline{\Gamma}$ are linear functions and \underline{m} is a nonlinear function of the state variables $\underline{x}(k)$; $\underline{w}(k)$ is the excitation noise and $\underline{v}(k)$ is the measurement noise of the system.

The plant noises are considered uncorrelated, zero-mean, and white.

The non-linear measurement equations can be linearized by expanding equation (2) around the best estimate at time k and using the first-order terms yielding

$$\underline{z}(k) = \underline{H}(k) \underline{x}(k) + \underline{v}(k)$$

where

$$\underline{H}(k) = \frac{\partial m}{\partial \underline{x}} \underline{x} = \hat{\underline{x}}(k/k-1) \quad (3)$$

$\hat{\underline{x}}(k/k)$ is the estimated value of the state at k after the k^{th} measurement and $\hat{\underline{x}}(k/k-1)$ is the predicted value of the state at time k before the k^{th} measurement.

The state error vector is

$$\hat{\underline{x}}'(k/k) = \hat{\underline{x}}(k/k) - \hat{\underline{x}}(k)$$

and the predicted error vector is

$$\hat{\underline{x}}'(k/k-1) = \hat{\underline{x}}(k/k-1) - \underline{x}(k)$$

The covariance of the state error matrix is

$$P(k/k) = E[\hat{\underline{x}}'(k/k) \hat{\underline{x}}'^T(k/k)]$$

and the predicted covariance of the state error matrix is

$$P(k/k-1) = E[\hat{\underline{x}}'(k/k-1) \hat{\underline{x}}'^T(k/k-1)] .$$

The state excitation matrix is

$$Q(k) = E[\underline{\Gamma}(k) \underline{w}(k) \underline{w}^T(k) \underline{\Gamma}^T(k)]$$

and the measurement noise covariance matrix is

$$R(k) = E[\underline{v}(k) \underline{v}^T(k)] .$$

The equations that made up the Kalman Filter used in this work are as follows:

$$P(k/k-1) = \underline{\Phi}(k) P(k/k) \underline{\Phi}^T(k) + Q(k)$$

$$G(k) = P(k/k-1) H^T(k) [H(k) P(k/k-1) H^T(k) + R(k)]^{-1}$$

$$P(k/k) = [I - G(k) H(k)] P(k/k-1)$$

$$\hat{\underline{x}}(k/k) = \hat{\underline{x}}(k/k-1) + G(k) [\underline{z}(k) - H(k) \underline{x}(k/k-1)]$$

$$\hat{\underline{x}}(k/k-1) = \underline{\Phi}(k) \hat{\underline{x}}(k/k)$$

$$\underline{z}(k) = \underline{m}(\underline{x}(k/k-1), k)$$

Since the only observations in this system are ranges,

the observation equation is

$$\underline{z}(k) = [x^2(k) + y^2(k)]^{1/2} ;$$

and from equation (3) we get

$$H(k) = \frac{x(k)}{x^2(k) + y^2(k)} \quad 0 \quad \frac{y(k)}{x^2(k) + y^2(k)} \quad 0 .$$

The covariance of estimation error, P , is an expression of the uncertainty in the estimation of the states. Considering only the estimation's position error, P_{position} can be expressed as

$$P_{\text{position}} = \begin{bmatrix} \sigma_x^2 & \sigma_x \sigma_y \\ \sigma_y \sigma_x & \sigma_y^2 \end{bmatrix}$$

Since the position estimation error is normally distributed, a curve of constant error probability can be defined by using the exponent of the normal distribution,

$$\frac{x^2}{\sigma_x^2} - \frac{2r_{xy}}{\sigma_x \sigma_y} + \frac{y^2}{\sigma_y^2}$$

This curve defines an ellipse. Graphically, for the given probability, the estimation may be anywhere in that ellipse.

III. CHOOSING THE BEST RANGER

To move from a simple Kalman Filter observer to the PLRS model, the first problem encountered was to choose the best ranger from which to take the measurement. In the previous work, [1], it was shown that the most useful measurement, the one causing the most reduction in the error ellipse, is obtained by observing the update unit from a point aligned with the major axis of the error ellipse of the update unit.

To find the ranger most closely aligned with the major axis of the update unit's error ellipse the orientation of the error ellipse must first be found using the following equation.

$$\theta = \frac{1}{2} \tan^{-1} \frac{2 \text{Cov}(x,y)}{\sigma_x^2 - \sigma_y^2}$$

This angle(θ) gives the angle between -90° and 90° that the x-axis of the ellipse makes with the x-axis of the co-ordinate system. Looking at the ellipse in this new posture one can find the new "Uncorrelated" variances that define the major and minor axes.

$$\sigma_{x'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} + \frac{\text{Cov}(x,y)}{\sin 2\theta} ,$$

$$\sigma_{y'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} - \frac{\text{Cov}(x,y)}{\sin 2\theta} ,$$

If σ_x^2 is greater than σ_y^2 the x-axis of the error ellipse is the major axis and θ is the angle we seek. If σ_y^2 is greater than σ_x^2 then the y-axis of the error ellipse is the major axis and the angle we seek is $\theta + 90^\circ$.

The bearing of the update unit from the ranger must then be found and it is simply

$$\beta = \text{Tan}^{-1} \frac{Y_U - Y_R}{X_U - X_R}.$$

The absolute value of the difference between θ , after proper correction, and β was chosen as the best alignment indicator; but to be aligned and to be 180° out of alignment is of equal value; therefore the absolute value of the cosine of the differences was used as the alignment indicator and the ranger found to have the largest indicator was chosen as the ranging unit for that measurement.

IV. PLRS SIMULATION

A. TWO RANGING UNITS

In previous work,[1], the PLRS simulation was setup for a jet aircraft flying Mach 1 in a constant 10 Km turn about the origin to act as the update unit for all measurements. Two stationary ranging units were placed at the origin and at 10Km north, 10Km east. Using a one second sample interval, the jet was described by the following matrices:

$$\phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\Gamma = \begin{bmatrix} 0.5 & 0 \\ 1 & 0 \\ 0 & 0.5 \\ 0 & 1 \end{bmatrix}$$

Its initial state was

$$\underline{x} = \begin{bmatrix} 0 \\ 0.333 \text{ Km/s} \\ 10 \text{ Km} \\ 0 \end{bmatrix}$$

Its initial covariance of error matrix, measurement noise covariance, and excitation forcing matrix were

$$P(1/0) = \begin{bmatrix} 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 10^{-4} & 0 & 0 \\ 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 0 & 0 & 10^{-4} \end{bmatrix}$$

and

$$R = 10^{-4}$$

with

$$Q = \begin{bmatrix} 2.5 \times 10^{-5} & 5 \times 10^{-5} & 0 & 0 \\ 5 \times 10^{-5} & 10^{-4} & 0 & 0 \\ 0 & 0 & 2.5 \times 10^{-5} & 5 \times 10^{-5} \\ 0 & 0 & 5 \times 10^{-5} & 10^{-4} \end{bmatrix}$$

Fig 2 is a display of its final runs. The filter tracked accurately and the error ellipses shown are twenty times their actual size to make them visible. Table 1 shows which was the ranging unit at each measurement time.

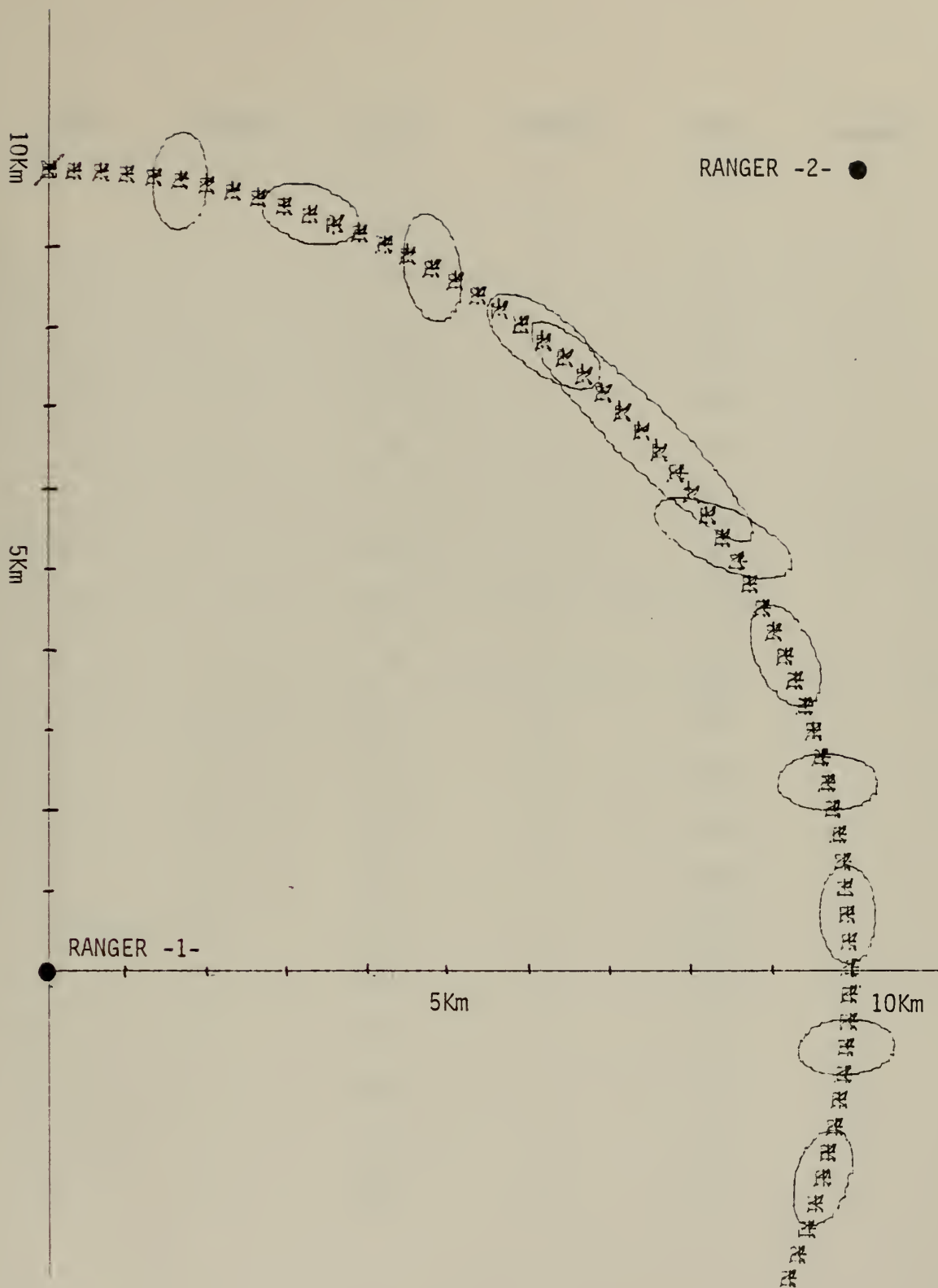


Figure 2 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING BETWEEN TWO STATIONARY RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	1	42	2
3	2	23	2	43	1
4	1	24	1	44	2
5	2	25	1	45	1
6	1	26	2	46	2
7	2	27	1	47	1
8	1	28	2	48	2
9	2	29	1	49	1
10	1	30	2	50	2
11	2	31	1	51	1
12	1	32	2	52	2
13	2	33	1	53	1
14	1	34	2	54	2
15	2	35	1	55	1
16	1	36	2	56	2
17	2	37	1	57	1
18	1	38	2	58	2
19	2	39	1	59	1
20	1	40	2	60	2

TABLE 1 - THE RANGER CHOSEN AT EACH TIME FOR THE PLRS TWO
STATIONARY RANGER SIMULATION

B. THREE RANGING UNITS

The first step of this study was to add a third ranging unit at 0 north, 10Km east. The algorithm was enlarged to include the additional unit and its comparison with the alignment indicators of the other ranging units.

It can be seen in Fig 3 that the size of the error ellipses were reduced in size in the mid-range area where the jet and the two original units were in line; and the third ranger provides the triangular measurement.

Table 2 shows the ranging unit chosen for the measurement at each time k.

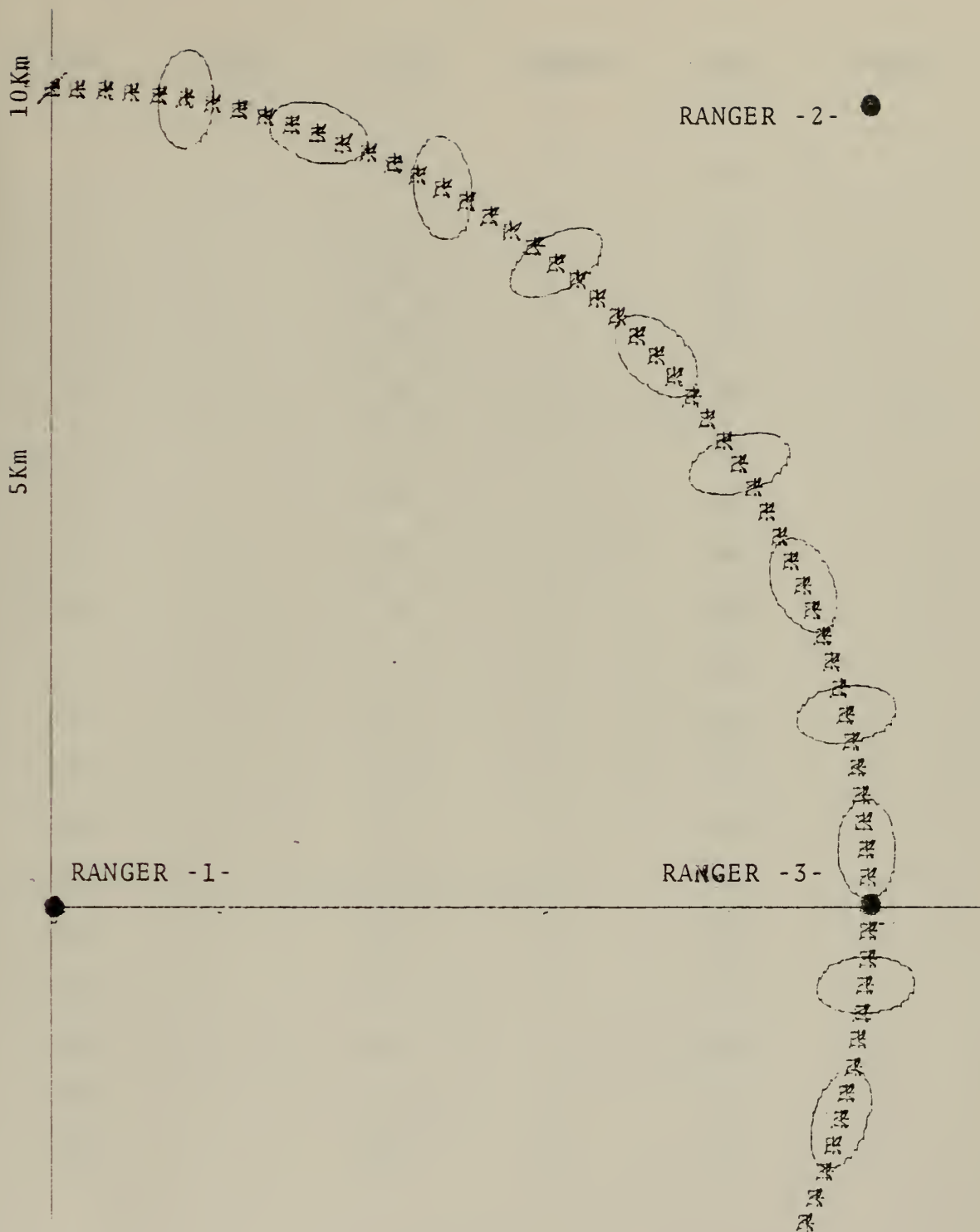


Figure 3 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE STATIONARY RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	3
3	2	23	2	43	1
4	1	24	3	44	3
5	2	25	1	45	1
6	1	26	3	46	3
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	1	30	3	50	2
11	2	31	1	51	1
12	1	32	3	52	3
13	2	33	1	53	1
14	3	34	3	54	3
15	2	35	1	55	1
16	3	36	3	56	3
17	2	37	1	57	1
18	3	38	3	58	3
19	2	39	1	59	1
20	3	40	3	60	3

TABLE 2 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
STATIONARY RANGER SIMULATION

C. RANGING UNITS IN MOTION

In the second step the rangers are given motion. The rangers at the origin and at 10Km north, 10Km east were to move north and south respectively at 3Kts as infantrymen. The ranger at 0 north, 10Km east was to move west at 120Kts as a helicopter. Again using one second sample intervals, their motion was defined using discrete linear state equations

$$x(k+1) = \phi(k) x(k) ,$$

where

$$\phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

with the initial states shown below;

$$x = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

$$x = \begin{bmatrix} 10 \\ 0 \\ 10 \\ -1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

$$\begin{array}{rcl}
 & 12 & \\
 x = & -5.555 \times 10^2 & \text{Km/s} \quad \text{HELICOPTER} \\
 & 0 & \\
 & 0 &
 \end{array}$$

It can be seen in Fig 4 that no system depreciation resulted from the motion of the rangers, Table 3 shows the ranging unit chosen for the measurement at each time,

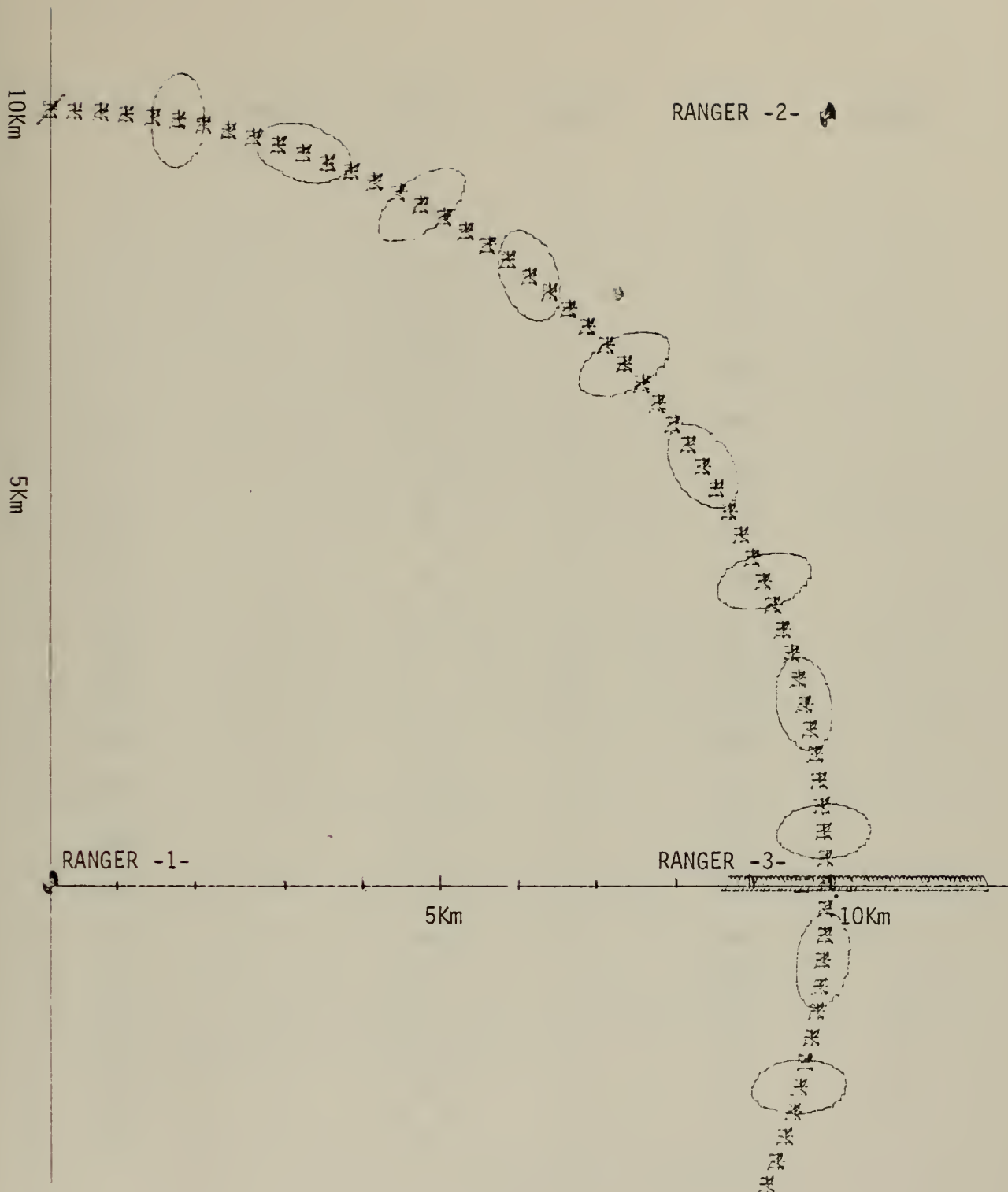


Figure 4 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE MOVING RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	3	41	3
2	1	22	2	42	1
3	2	23	3	43	2
4	1	24	2	44	1
5	2	25	3	45	2
6	1	26	1	46	1
7	2	27	3	47	2
8	1	28	1	48	1
9	2	29	3	49	2
10	1	30	1	50	1
11	2	31	3	51	2
12	1	32	1	52	1
13	3	33	3	53	2
14	1	34	1	54	1
15	3	35	3	55	2
16	2	36	1	56	1
17	3	37	3	57	2
18	2	38	1	58	1
19	3	39	3	59	2
20	2	40	1	60	1

TABLE 3 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGER SIMULATION

D. SOURCE OF MEASUREMENT NOISE

In the above simulations the position of the ranging unit has been assumed to be exact; while in actual application the ranging units will have covariances of estimation error defining an error ellipse; and the ranging unit might be anywhere within that ellipse. To bring this position uncertainty into the simulation, the radius of the error ellipse along the bearing from the ranging unit to the update unit was defined as the covariance of measurement error.

The equation for the radius of an ellipse is a function of the major axis, the minor axis, and the angle at which the measurement is made. To find the measurement noise covariance, or the ellipse radius, σ_x^2 and σ_y^2 must be compared and the larger defined as M_j , the major axis, and the smaller defined as M_n , the minor axis. The angle, α , at which the radius is determined is measured from the major axis and thus is calculated as the difference between θ and β . Fig 5 shows the geometry of the calculation of the covariance of measurement noise. The equation for R and the radius squared of the ellipse is:

$$R = r^2 = \frac{M_j M_n}{M_j \sin^2 \alpha + M_n \cos^2 \alpha}$$

It can be seen in Fig 6 that performance was improved slightly using the covariance of estimation error as the sole source of measurement noise.

Table 4 shows the ranger chosen at each time for the three moving rangers with position uncertainty simulation.

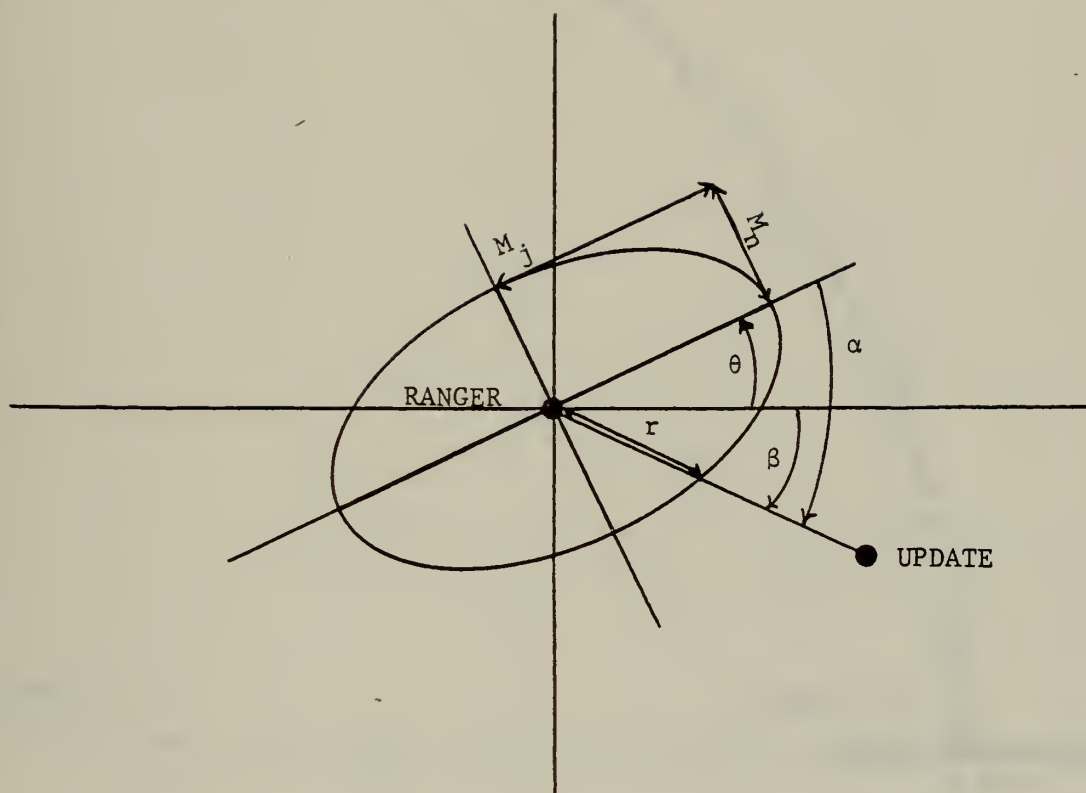


Figure 5 - r IS THE RADIUS OF THE ERROR ELLIPSE - $r^2 = R$
 IS THE COVARIANCE OF MEASUREMENT NOISE

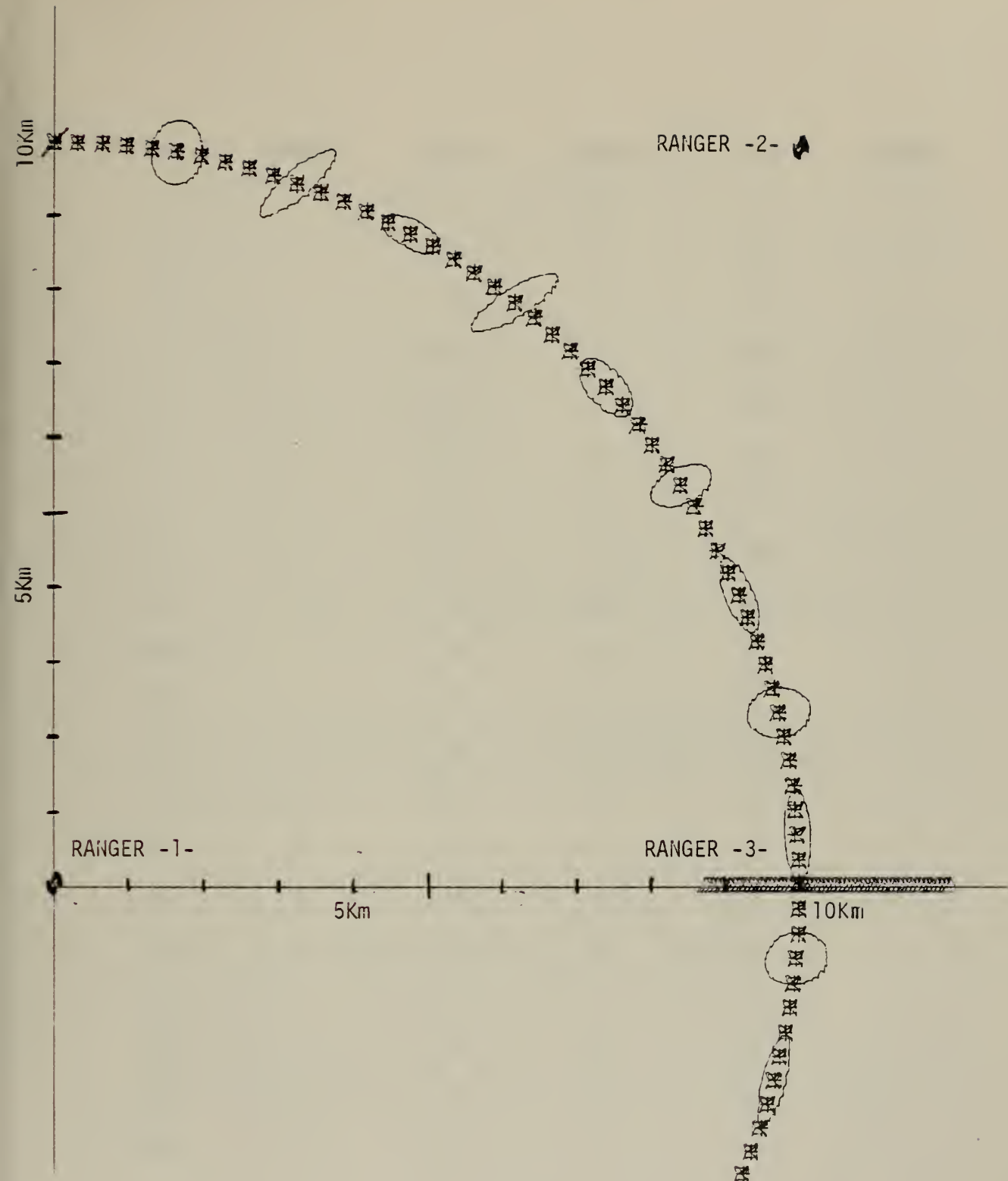


Figure 6 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE MOVING RANGERS WITH POSITION
UNCERTAINTY

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	2
3	2	23	2	43	1
4	1	24	3	44	2
5	2	25	1	45	1
6	1	26	3	46	2
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	3	30	3	50	2
11	1	31	1	51	1
12	3	32	3	52	2
13	1	33	1	53	1
14	3	34	3	54	2
15	1	35	1	55	1
16	3	36	3	56	2
17	1	37	1	57	1
18	3	38	3	58	2
19	2	39	1	59	1
20	3	40	3	60	2

TABLE 4 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGERS WITH POSITION UNCERTAINTY SIMULATION

V. CONCLUSION

The placement of the third ranger showed the value of triangulation of the rangers. The closer to normal the bearings of the rangers are to each other, the better the results of consecutive ranges.

The allowance for motion and the representation of the ranger's position uncertainty as the source of measurement error were important steps toward full simulation of the system; and they were accomplished without degradation of performance.

A better simulation may be to represent the measurement error as the ranger's position uncertainty plus some system measurement error.

Still to be accomplished is the ability to update all units at each ranging, and to provide a gating system that will demand more frequent updates for faster moving units and less frequent updates for slower units.

A program listing of the three moving rangers with position uncertainty is included with an annotated data deck.

C	DC 23 I=1,N	MCSP0204
	DO 23 J=1,N	MCSP0205
23	PHIS(I,J) = PHI(I,J)	MCSP0207
	WRITE (6,131)	MCSP0208
	CALL MWRITE (PHI,N,N)	MCSP0210
C		MCSP0211
C		MCSP0212
	CALL MREAD (H,M,N)	MCSP0213
	DO 25 I=1,M	MCSP0215
	DO 25 J=1,N	MCSP0217
25	HS(I,J) = H(I,J)	MCSP0219
	WRITE (6,132)	MCSP0220
	CALL MWRITE (H,M,N)	MCSP0222
C		MCSP0223
C		MCSP0224
	CALL MREAD (R,M,M)	MCSP0225
	WRITE (6,133)	MCSP0227
	CALL MWRITE (R,M,M)	MCSP0228
C		MCSP0229
C		MCSP0230
	CALL MREAD (COVW,IN,IN)	MCSP0231
	WRITE (6,134)	MCSP0233
	CALL MWRITE (COVW,IN,IN)	MCSP0234
	CALL MREAD (GAMMA,N,IN)	MCSP0235
C		MCSP0244
	DO 30 I=1,N	MCSP0245
	DO 30 J=1,IN	MCSP0246
30	GAMMAS(I,J) = GAMMA(I,J)	MCSP0248
	WRITE (6,136)	MCSP0249
	CALL MWRITE (GAMMA,N,IN)	MCSP0251
C		MCSP0252
C		MCSP0253
	CALL MREAD (PKKM1,N,N)	MCSP0254
	WRITE (6,137)	MCSP0256
	CALL MWRITE (PKKM1,N,N)	MCSP0257
C		MCSP0258
C		MCSP0259
	DO 311 K=2,NR	CH3*****1
	CALL MREAD (PRR,N,N)	CH3*****2
	DO 310 I=1,N	CH3*****3
	DO 310 J=1,N	CH3*****4
310	PR(I,J,K) = PRR(I,J)	CH3*****5
311	CONTINUE	CH3*****6
C		
C		
	CALL VREAD (SIGV,M)	MCSP0260
	WRITE (6,138)	MCSP0262
		MCSP0263


```

C      CALL VWRITE (SIGV,M)
C
C      DO 340 I=1,NR
C      READ (5,144) (XHATZ(I,J),J=1,N)
C      WRITE (6,140)
C      340 WRITE (6,146) (XHATZ(I,J),J=1,N)
C
C      36 DO 360 I=1,NR
C      READ (5,144) (XS(I,J,1),J=1,N)
C      INITIAL CONDITION HAS BEEN READ
C      WRITE (6,143)
C      360 WRITE (6,146) (XS(I,J,1),J=1,N)
C
C      38 CALL TRACK
C
C      DO 390 K=1,NR
C      WRITE (6,145)
C      39 WRITE (6,146) (XS(K,I,1),I=1,N)
C      WRITE (6,146) (XS(K,I,NSAM),I=1,N)
C      390 CONTINUE
C
C      THE FOLLOWING SECTION PREPARES FOR THE MONTE CARLO LOOP
C      FORM NXN IDENTITY MATRIX IN DOUBLE PRECISION
C
C      DO 41 I=1,N
C      DO 41 J=1,N
C      EI(I,J) = 0.00
C      41 IF (I.EQ.J) EI(I,J)=1.00
C
C      GIVEN THE MATRIX GAMMA AND THE COVARIANCE OF W COMPUTE Q
C      USING DOUBLE PRECISION ARITHMETIC
C
C      CALL QMAT
C      WRITE (6,135)
C      CALL MWRITE (Q,N,N)
C
C      SET UP ARRAYS FOR COMPUTING STATISTICS
C
C      DO 48 I=1,NR
C      DO 48 K=1,NSAM
C      DC 48 J=1,N

```

```

MC SP0264
MC SP0265
MC SP0272
CH200006
CH200007
MC SP0275
CH200008
MC SP0277
MC SP0292
CH200009
CH200010
MC SP0294
MC SP0295
CH200011
MC SP0302
MC SP0247
MC SP0304
MC SP0250
MC SP0307
CH200012
MC SP0308
CH200013
CH200014
CH200015

MC SP0313
MC SP0314
MC SP0221
MC SP0316
MC SP0317
MC SP0318
MC SP0320
MC SP0321
MC SP0322
MC SP0323
MC SP0324
MC SP0325
MC SP0319
MC SP0327
MC SP0328
MC SP0329
MC SP0356
MC SP0357
MC SP0358
CH200016
MC SP0359
MC SP0360
MC SP0361

```



```

C      XM(I,J,K) = 0.
C      ERR(I,J,K) = 0.
C
C      DO 48 L=1,N
C      48  VAR(J,L,K) = 0.
C
C      BEGIN MAIN ITERATION LOOP HERE
C      DC 54 ITER=1,NENS
C
C      49 DO 50 I=1,N
C      50  XHKM1(I) = XHATZ(1,I)
C
C      DO 54 K=1,NSAM
C      FORM NOISY MEASUREMENT FROM TRUE STATE VALUE
C
C      DO 51 I=1,N
C      51  X(I) = XS(1,I,K)
C      CALL GAIN
C
C      DO 52 I=1,N
C      DO 52 J=1,M
C      52  GKS(I,J,K) = G(I,J)
C
C      UPDATE THE STATE ESTIMATE
C
C      53 CALL ESTIM
C      UPDATE RUNNING SUMS USED IN COMPUTING STATISTICS
C      CALL STAT
C
C      54 CCNTINUE
C
C      DIVIDE RUNNING SUMS COMPUTED BY SUBROUTINE STAT BY ENSEMBLE
C      SIZE TO COMPUTE STATISTICS
C      ENS = NENS
C
C      DO 56 K=1,NSAM
C      DO 56 J=1,N
C      55  ERR(1,J,K) = ERR(1,J,K)/ENS
C

```

CH2000017
 CH2000019
 MCSP0364
 MCSP0365
 MCSP0366
 MCSP0367
 MCSP0368
 MCSP0369
 MCSP0370
 MCSP0371
 MCSP0372
 MCSP0375
 MCSP0376
 CH200018
 MCSP0378
 MCSP0379
 MCSP0380
 MCSP0381
 MCSP0382
 MCSP0383
 MCSP0384
 CH200020
 MCSP0386
 MCSP0396
 MCSP0397
 MCSP0398
 MCSP0400
 MCSP0401
 MCSP0402
 MCSP0403
 MCSP0404
 MCSP0405
 MCSP0406
 MCSP0407
 MCSP0408
 MCSP0409
 MCSP0411
 MCSP0414
 MCSP0415
 MCSP0416
 MCSP0417
 MCSP0418
 MCSP0419
 MCSP0420
 MCSP0421
 MCSP0422
 MCSP0423
 CH2000022


```

C      REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
3GAMMAS(4,4), PHIS(4,4,60), XS(4,4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4,4), Z(4), V(4), SIGV(4),
5XHATZ(4,4), YZ(60), PX(10), PY(10), PR(4,4,4),
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
      CALL PROD (GAMMA, COVW, N, IN, IN, TEMP)
      CALL TRANS (GAMMA, N, IN, TEMP1)
      CALL PROD (TEMP, TEMP1, N, IN, N, Q)
      RETURN
      END
      SUBROUTINE QON
      IF Q IS TO BE COMPUTED ON-LINE (IFLQ.NE.0) IT IS DONE
      IN THIS SUBROUTINE
      REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
3GAMMAS(4,4), PHIS(4,4,60), XS(4,4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4,4), Z(4), V(4), SIGV(4),
5XHATZ(4,4), YZ(60), PX(10), PY(10), PR(4,4,4),
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
      THE APPROPRIATE STATEMENTS FOR COMPUTING Q ON-LINE MUST
      BE INSERTED HERE BY THE USER
      RETURN
      END
      SUBROUTINE RON
      IF R IS TO BE COMPUTED ON-LINE (IFLR.NE.0) IT IS DONE
      IN THIS SUBROUTINE
      REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
3GAMMAS(4,4), PHIS(4,4,60), XS(4,4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4,4), Z(4), V(4), SIGV(4),
5XHATZ(4,4), YZ(60), PX(10), PY(10), PR(4,4,4),
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR

```

C

CC

CCCC

CCCC

CCCC


```

C      THE APPROPRIATE STATEMENTS FOR COMPUTING R ON-LINE MUST
C      BE INSERTED HERE BY THE USER
C
C      RETURN
C      END
C
C      SUBROUTINE STAT
C
C      THIS SUBROUTINE COMPUTES RUNNING SUMS USED IN DETERMINING THE
C      SAMPLE STATISTICS OF THE TRACK AND ESTIMATION ERRORS. IN THE DEFAULT
C      OPTION (ISTAT.EQ.0) THE STATISTICS TO BE COMPUTED ARE MEAN OF
C      TRACK, MEAN OF ESTIMATION ERROR AND VARIANCE OF ESTIMATION
C      ERROR. IF (ISTAT.NE.0) THE OFF-DIAGONAL TERMS IN THE COVARIANCE OF
C      ESTIMATION ERROR MATRIX ARE ALSO COMPUTED.
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), HS(4,4), GK(4,4,60), X(4,4),
C      4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), XHKKM1(4,4), VTMP(4,4), SIGW(4,4),
C      5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), V(4), SIGV(4),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
C      DIMENSION EXH(3)
C      IF (ITER.NE.1) GO TO 2
C      IF (ITER.NE.1) GO TO 4
C
C      DO 1 J=1,N
C      1 XM(1,J,K) = XS(1,J,K)
C
C      GO TO 4
C      2 CONTINUE
C
C      DO 3 J=1,N
C      3 XM(1,J,K) = XM(1,J,K)+XS(1,J,K)
C
C      4 CCNTINUE
C
C      DO 5 J=1,N
C      EXH(J) = XHKK(J)-XS(1,J,K)
C      ERR(1,J,K) = ERR(1,J,K)+EXH(J)
C      5 VAR(J,J,K) = VAR(J,J,K)+EXH(J)**2
C
C      IF (ISTAT.EQ.0) RETURN
C
C      DO 6 L=2,N
C      LM1 = L-1
C
C

```

```

MCSP0820
MCSP0821
MCSP0822
MCSP0823
MCSP0824
MCSP0825
MCSP0826
MCSP0827
MCSP0828
MCSP0829
MCSP0830
MCSP0831
MCSP0832
CH3*****
MCSP0834
MCSP0835
CH200034
CH200035
MCSP0838
CH200004
CH2
MCSP0841
MCSP0842
MCSP0843
MCSP0844
MCSP0845
CH200037
MCSP0847
MCSP0848
MCSP0849
MCSP0850
MCSP0851
CH200038
MCSP0853
MCSP0854
MCSP0855
MCSP0856
CH200039
CH2
MCSP0859
MCSP0860
MCSP0861
MCSP0862
MCSP0863
MCSP0864
MCSP0865

```



```

C      DO 6 J=1,LM1
C      6 VAR(L,J,K) = VAR(L,J,K)+EXH(L)*EXH(J)
C      RETURN
C      END
C      SUBROUTINE XZERO
C      THIS SUBROUTINE GENERATES THE INITIAL STATE VALUE FROM A NORMAL
C      RANDOM NUMBER GENERATOR. IT IS ASSUMED THAT THE INITIAL STATE
C      HAS COMPONENTS THAT ARE INDEPENDENT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),PHI(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),PKK(4,4),G(4,4),
C      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
C      3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4,4),X(4,4),
C      4SIGXZ(4,4),XZMEAN(4,4),XHKK(4,4),XHKKM1(4,4),VTMP(4,4),Z(4,4),V(4,4),SIGV(4,4),
C      5XHATZ(4,4),YZ(60),PX(10),PY(10),PR(4,4,4),IEST,ND,NR
C      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND,NR
C      CALL SNORM (IXZ,X,N)
C
C      DO 1 I=1,N
C      1 XS(1,I,1) = SIGXZ(1)*X(1)+XZMEAN(1)
C      RETURN
C      END
C      SUBROUTINE ADD (A,B,N,M,C)
C      THIS SUBROUTINE ADDS THE NXM MATRICES A AND B, STORING THE
C      RESULT IN C
C      REAL*8 A,B,C
C      DIMENSION A(4,4),B(4,4),C(4,4)
C
C      DO 1 I=1,N
C      DO 1 J=1,M
C      1 C(I,J) = A(I,J)+B(I,J)
C      RETURN
C      END
C      SUBROUTINE MREAD (A,N,M)
C      8D10.5. THE ENTRIES IN THE FIRST ROW OF A ARE READ FIRST, THEN
C      THIS SUBROUTINE READS AN NXM MATRIX A ACCORDING TO THE FORMAT
C      THE ENTRIES IN THE SECOND ROW, AND SO ON.
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DC 1 I=1,N
C      1 READ (5,2) (A(I,J),J=1,M)
C      RETURN

```

MCSP0866
 MCSP0867
 MCSP0868
 MCSP0869
 MCSP0870
 MCSP0934
 MCSP0935
 MCSP0936
 MCSP0937
 CH3*****
 MCSP0939
 MCSP0940
 CH200040
 CH200041
 MCSP0943
 CH20000*
 CH2
 MCSP0946
 MCSP0947
 MCSP0948
 CH2
 MCSP0950
 MCSP0951
 MCSP0952
 MCSP0953
 MCSP0954
 MCSP0955
 MCSP0956
 MCSP0957
 MCSP0958
 MCSP0959
 MCSP0960
 MCSP0961
 MCSP0962
 MCSP0963
 MCSP0964
 MCSP0965
 MCSP0966
 MCSP0968
 MCSP0967
 MCSP0969
 MCSP0970
 MCSP0971
 MCSP0972
 MCSP0973
 MCSP0974
 MCSP0975
 MCSP0976


```

C      2 FORMAT (8F10.0)
C      END
C      SUBROUTINE MWRITE (A,N,M)
C      THIS SUBROUTINE WRITES THE ENTRIES OF THE NXM MATRIX A
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DC 1 I=1,N
C      1 WRITE (6,2) (A(I,J),J=1,M)
C
C      RETURN
C
C      2 FORMAT (9(2X,1PE12.5))
C      END
C      SUBROUTINE PROD (A,B,N,M,L,C)
C      THIS SUBROUTINE COMPUTES THE MATRIX PRODUCT AB AND STORES THE
C      RESULT IN C
C      A = NXM, B = MXL, C = NXL
C      REAL*8 A,B,C,T
C      DIMENSION A(4,4),B(4,4),C(4,4),T(4,4)
C
C      DO 1 I=1,N
C
C      DO 1 J=1,L
C      1 T(I,J) = 0.0
C
C      DO 2 I=1,N
C
C      DO 2 J=1,L
C
C      DO 2 K=1,M
C      2 T(I,J) = T(I,J)+A(I,K)*B(K,J)
C
C      DO 3 I=1,N
C
C      DO 3 J=1,L
C      3 C(I,J) = T(I,J)
C
C      RETURN
C      END
C      SUBROUTINE SUB (A,B,N,M,C)
C      THIS SUBROUTINE SUBTRACTS THE NXM MATRIX B FROM THE NXM MATRIX
C      A AND STORES THE RESULT IN C
C      REAL*8 A,B,C
C      DIMENSION A(4,4),B(4,4),C(4,4)

```

MC SP0977
 MC SP0978
 MC SP0979
 MC SP0980
 MC SP0981
 MC SP0982
 MC SP0983
 MC SP0984
 MC SP0985
 MC SP0986
 MC SP0987
 MC SP0988
 MC SP0989
 MC SP0990
 MC SP0991
 MC SP0992
 MC SP0993
 MC SP0994
 MC SP0995
 MC SP0996
 MC SP0997
 MC SP0998
 MC SP0999
 MC SP1000
 MC SP1001
 MC SP1002
 MC SP1003
 MC SP1004
 MC SP1005
 MC SP1006
 MC SP1007
 MC SP1008
 MC SP1009
 MC SP1010
 MC SP1011
 MC SP1012
 MC SP1013
 MC SP1014
 MC SP1015
 MC SP1016
 MC SP1017
 MC SP1018
 MC SP1019
 MC SP1020
 MC SP1021
 MC SP1022
 MC SP1023
 MC SP1024


```

C      DC 1 I=1,N
C
C      DO 1 J=1,M
C      1 C(I,J) = A(I,J)-B(I,J)
C
C      RETURN
C      END
C      SUBROUTINE TRANS (A,N,M,C)
C      THIS SUBROUTINE FORMS THE MATRIX TRANSPOSE CF A STORING THE
C      RESULT IN C
C      A = NXM, C = MXN
C      REAL*8 A,C
C      DIMENSION A(4,4),C(4,4)
C
C      DO 1 I=1,N
C
C      DC 1 J=1,M
C      1 C(J,I) = A(I,J)
C
C      RETURN
C      END
C      SUBROUTINE VADD (X,Y,N,Z)
C      THIS SUBROUTINE COMPUTES THE SUM OF THE N-VECTORS X AND
C      Y AND STORES THE RESULT IN THE N-VECTOR Z
C
C      REAL*4 X(4),Y(4),Z(4)
C
C      DO 1 I=1,N
C      1 Z(I) = X(I)+Y(I)
C
C      RETURN
C      END
C      SUBROUTINE VPROD (A,X,M,N,Y)
C      THIS SUBROUTINE COMPUTES THE PRODUCT OF THE MXN MATRIX
C      A AND THE N-VECTOR X AND STORES THE RESULT IN THE
C      M-VECTOR Y
C
C      REAL*4 A(4,4),X(4),Y(4),T(4)
C
C      DO 1 I=1,M
C      T(I) = 0.00
C
C      DO 1 J=1,N
C      1 T(I) = T(I)+A(I,J)*X(J)
C
C

```

MCSP1025
 MCSP1026
 MCSP1027
 MCSP1028
 MCSP1029
 MCSP1030
 MCSP1031
 MCSP1032
 MCSP1033
 MCSP1034
 MCSP1035
 MCSP1036
 MCSP1037
 MCSP1038
 MCSP1039
 MCSP1040
 MCSP1041
 MCSP1042
 MCSP1043
 MCSP1044
 MCSP1045
 MCSP1046
 MCSP1047
 MCSP1048
 MCSP1049
 MCSP1050
 MCSP1051
 MCSP1052
 MCSP1053
 MCSP1054
 MCSP1055
 MCSP1056
 MCSP1057
 MCSP1058
 MCSP1059
 MCSP1060
 MCSP1061
 MCSP1062
 MCSP1063
 MCSP1064
 MCSP1065
 MCSP1066
 MCSP1067
 MCSP1068
 MCSP1069
 MCSP1070
 MCSP1071
 MCSP1072

MCSP1073
MCSP1074
MCSP1075

MCSP1076
MCSP1077
MCSP1078
MCSP1079
MCSP1080
MCSP1081
MCSP1082
MCSP1083

DO 2 I=1,M
2 Y(I) = T(I)

C

RETURN

END
SUBROUTINE VREAD (V,N)

C

THIS SUBROUTINE READS THE N-DIMENSIONAL S.P. VECTOR V

C

DIMENSION V(4)
READ (5,1) (V(I),I=1,N)

RETURN
1 FORMAT (8F10.0)

END
SUBROUTINE VSUB (X,Y,N,Z)
REAL*4 X(4),Y(4),Z(4)

DO 1 I=1,N
1 Z(I) = X(I)-Y(I)

RETURN
END
SUBROUTINE VWRITE (V,N)
DIMENSION V(4)
WRITE (6,1) (V(I),I=1,N)

RETURN
1 FORMAT (9(2X,1PE12.5))

END

SUBROUTINE TRACK
IF TRACK IS TO BE GENERATED ON-LINE IT IS DCNE IN THIS SUBROUTINE
IN THE DEFAULT OPTION (ITRK.EQ.0) THE TRACK IS GENERATED
FROM THE STANDARD LINEAR DIFFERENCE EQUATION

C

X(K+1)=PHI*X(K)+GAMMA*W(K)

C

REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),XZ(60),YZ(60),PX(10),PV(10),PR(4,4,4),IEST,ND,NK
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IST,ND,NK
DIMENSION W(3)

TO GENERATE A SINGLE TRAJECTORY AND STORE IT IN THE ARRAY
XS(I,K),I=1,N,K=2,NSAM (NOTE THAT IF A SINGLE TRAJECTORY IS TO BE
GENERATED, THE INITIAL CONDITION HAS BEEN READ IN AND STORED
IN XS(I,1),I=1,N)

C

C

C

C

MCSP0871
MCSP0872
MCSP0873
MCSP0874
MCSP0875
MCSP0876
MCSP0877
CH3*****
MCSP0879
MCSP0666
CH2000043
CH2000044
MCSP0883
CH20000#
CH2
MCSP0886
MCSP0913
MCSP0914
MCSP0915
MCSP0916
MCSP0917


```

TPI = 2.*3.14159265
DC 5 K=2, NSAM
EKML = K-1
T = 1.0*EKML
A=0.033333*T
IF(A.LT.TPI) GO TO 10
MM=A/TPI
FM=MM
A = A - FM*TPI
10 CCNTINUE
XS(1,1,K)=10.*SIN(A)
XS(1,2,K)=.3333*COS(A)
XS(1,3,K)=10.*COS(A)
XS(1,4,K)=-.3333*SIN(A)
DO 7 I=2,NR
EKML = K-1
XS(1,1,EKML) = XS(1,2,1)
XS(1,2,K) = XS(1,2,1)
XS(1,3,EKML) = XS(1,4,1)
XS(1,4,K) = XS(1,4,1)
7 CCNTINUE
C
RETURN
END
SUBROUTINE MEAS
THIS SUBROUTINE STARTS WITH THE TRUE STATE VALUE XS
AND ADDS ZERO-MEAN WHITE GAUSSIAN NOISE TO H*XS TO
GENERATE A NOISY VECTOR OF MEASUREMENTS Z.
C
C
C
C
REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4),
1TEMP(4,4,60), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), IEST, ND, NR
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IV, IW, I, XZ, IV, IW, IEST, ND, NR
ALPHA = XS(1,3,K)
BETA = XS(1,1,K)
Z(1) = SQRT(ALPHA**2+BETA**2)
Z(2) = ATAN2(ALPHA, BETA)
CALL SNORM (IV,V,M)
C
DC 1 I=1,M
1 V(I) = SIGV(I)*V(I)
C
CALL VADD (Z,V,M,Z)

```

MCSP0918
MCSP0919

CH2000046
CH2000047
CH2000048
CH2000049
CH2000050
CH2000051
CH2000053
CH2000054
CH2000055
CH2000056
CH2000057
MCSP0925
MCSP0926
MCSP0933
MCSP0734
MCSP0735
MCSP0736
MCSP0737
MCSP0738
MCSP0739
CH3*****
MCSP0741
MCSP0742
CH2000058
CH2000059
MCSP0745
CH200000*
CH20000061
CH2000062
MCSP0750
MCSP0751
MCSP0752
MCSP0753
MCSP0754
MCSP0755
MCSP0756
MCSP0757


```

C      ALPHA = Z(1)*COS(Z(2))
C      BETA = Z(1)*SIN(Z(2))
C      XZ(K)=ALPHA
C      YZ(K)=BETA
C      RETURN
C      END
C      SUBROUTINE GAIN
C
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), HS(4,4,60), GK(4,4), SIGW(4,4), X(4,4),
C      4SIGXZ(4,4), XZMEAN(4,4), XHKKM1(4,4), VTMP(4,4), Z(4,4), V(4,4), SIGV(4,4),
C      5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
C      DIMENSION BE(4), ER(4)
C
C      G(K) = P(K/K-1)*HT*(H*P(K/K-1)*HT + R)
C      DC 300 I=1,4
C      DO 300 J=1,4
C      300 PKKS(I,J,K)=PKKM1(I,J)
C
C      IF(DABS(PKKM1(1,1)-PKKM1(3,3)).GT.0) GO TO 11
C      PKKM1(1,1)=PKKM1(3,3)+0.000001
C      11 CONTINUE
C
C      FINE UPDATE UNIT'S ELLIPSE ORIENTATION
C
C      THE=0.5*DATAN(2.*PKKM1(1,3)/(PKKM1(1,1)-PKKM1(3,3)))
C      IF(ABS(THE).GT.0) GO TO 10
C      THE=0.00001
C      10 CONTINUE
C
C      FINE UNCOUPLED VARIANCES
C
C      SIG2X=(PKKM1(1,1)+PKKM1(3,3))/2.+PKKM1(1,3)/SIN(2.*THE)
C      SIG2Y=(PKKM1(1,1)+PKKM1(3,3))/2.-PKKM1(1,3)/SIN(2.*THE)
C
C      ADJUST THETA
C
C      IF(SIG2X*GE.SIG2Y) GO TO 63
C      THE=THE+3.14159265/2.
C
C      CALCULATE BEARING
C
C      DC 9 IN=1,3

```

MCSP0758
MCSP0759

MCSP0762
MCSP0763
MCSP0216
MCSP0695
MCSP0218
CH3***#
MCSP0697
MCSP0698
CH200063
CH200064
MCSP0701
CH20000*
CH2

MCSP0704
MCSP0705

PLR05810

PLR05660
PLR05870
PLR05880

PLR05930
PLR05940
PLR05950

PLR05980
PLR05990
PLR06000

CH200066

CH2000067
CH2000068
CH2000069
CH2000070

```

IO = IN + 1
IF (ABS(XHKKM1(1)-XS(IO,1,K)).GT.0) GO TO 9
XHKKM1(1) = 0.000001+XS(IO,1,K)
BE(IN)=ATAN((XHKKM1(3)-XS(IO,3,K))/(XHKKM1(1)-XS(IO,1,K)))
9 CONTINUE
63 DO 4 IN=1,3
66 DO 4 IN=1,3
4 ER(IN)=ABS(TH-BE(IN))

```

C
C
C

CHCOSE BEST RANGER

```

IF (ABS(COS(ER(1))) .LE. ABS(COS(ER(2)))) GO TO 7
IF (ABS(COS(ER(1))) .LE. ABS(COS(ER(3)))) GO TO 70
IN=1

```

```

70 GO TO 8
IN=2
7 IF (ABS(COS(ER(2))) .LE. ABS(COS(ER(3)))) GO TO 70

```

```

70 GO TO 8
IN=3
8 XIN=IN
IC=IN + 1

```

C
C
C

CALCULATE H

```

RR = ((XHKKM1(1)-XS(IO,1,K))**2+(XHKKM1(3)-XS(IO,3,K))**2)**.5
WRITE (6,22)
22 FORMAT(/,6X,'THE',12X,'SIG2X',8X,'SIG2Y',10X,'BE(1)',8X,'BE(2)',
18X,'XIN',10X,'ER(1)',9X,'ER(2)',10X,'RR')
WRITE (6,146) THE,SIG2X,SIG2Y,BE(1),BE(2),XIN,ER(1),ER(2),RR
146 FORMAT (9(2X,1PE12.5),/)

```

```

H(1,1)=(XHKKM1(1)-XS(IO,1,K))/RR
H(1,3) = (XHKKM1(3)-XS(IO,3,K))/RR
IF (DABS(PR(1,1,IN)-PR(3,3,IN)).GT.0) GO TO 20
PR(3,3,IN) = PR(1,1,IN)+0.000001
20 CONTINUE

```

C
C
C

FIND RANGER'S ERROR ELLIPSE ORIENTATION (THER)

```

THER = 0.5*ATAN(2.*PR(1,3,IN)/(PR(1,1,IN)-PR(3,3,IN)))
IF (ABS(THER).GT.0) GO TO 19
THER = 0.00001
19 SIG2XR = (PR(1,1,IN) + PR(3,3,IN)) / 2. + PR(1,3,IN) / SIN(2.*THER
1)

```

C
C
C

CALCULATE RANGER'S UNCORELATED VARIANCES

```

SIG2YR = (PR(1,1,IN) + PR(3,3,IN)) / 2. - PR(1,3,IN) / SIN(2.*THERCH3****10
1)
CH3****11
IF (SIG2YR.GE.0.) GO TO 21
CH3?????

```

PLR06200
PLR06210
PLR06220
CH2000071
CH3*****
CH3*****
CH3*****
MCSP0634
CH200072
CH200073
CH3*****
CH3*****
CH3*****
PLR06300
PLR06310
CH3*****7
CH3*****
CH3*****8
CH3*****9


```

END
SUBROUTINE ESTIM
THIS SUBROUTINE UPDATES THE STATE ESTIMATE. IN THE DEFAULT
CONDITION (TEST.EQ.0) THE STANDARD EQUATIONS
XHAT(K/)=XHAT(K/K-1)+G(K)*(Z(K)-H(K)*XHAT(K/K-1))
X+AT(K+1/K)=PHI*XHAT(K/K)
ARE EVALUATED
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),IEST,ND,NR
6N,NSAM,IQ,M,ITER,IIRK,IN,ISTAT,K,ITRO,IXZ,IW,IW,ARRAY GK
TAKE THE APPROPRIATE GAIN AND STORE IN THE ARRAY GK
XIN=IN + 1
IC = IN + 1
DO 1 I=1,N
DO 1 J=1,M
1 GK(I,J) = GKS(I,J,K)
CALL VPROD (HS, XHKKM1, M, N, VTMP)
VTMP(1)=((XHKKM1(1)-XS(10,1,K))*2+(XHKKM1(3)-XS(10,3,K))*2)**.5
Z(1) = ((XZ(K)-XS(10,1,K))*2+(YZ(K)-XS(10,3,K))*2)**.5
CALL VSUB (Z,VTMP,M,VTMP)
CALL VPROD (GK,VTMP,N,M,VTMP)
CALL VADD (XHKKM1,VTMP,N,XHKK)
XHAT(K/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKK
CALL VPROD (PHIS,XHKK,N,N,XHKKM1)
XHAT(K+1/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKKM1
RETURN
END
SUBROUTINE PRT
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),

```

MCSP0733
MCSP0206
MCSP0655
MCSP0209
MCSP0656
MCSP0657
MCSP0658
MCSP0659
MCSP0660
MCSP0661
MCSP0662
MCSP0663
CH3****
MCSP0665
MCSP0666
CH200074
CH200075
MCSP0669
CH20000*
CH2
MCSP0672
MCSP0673
MCSP0675

CH2
MCSP0674
MCSP0676
MCSP0677
MCSP0678
MCSP0680
CH200077
CH200078
MCSP0681
MCSP0682
MCSP0683
MCSP0684
MCSP0685
MCSP0686

MCSP0688
MCSP0689
MCSP0694
CH3****
MCSP0879
MCSP0666
CH200079
CH200080


```

4 SIGXZ(4), XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),EST,ND,NR
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,WRITE(6,147)

```

MCSP0012
CH20000*
CH2
MCSP0446

```

WRITE GAINS, THEORETICAL COVARIANCES OF ESTIMATION ERROR
WRITE (6,148)

```

MCSP0447
MCSP0450
MCSP0451

```

DC 59 K=1, NSAM
WRITE (6,149) K

```

MCSP0452
MCSP0453
MCSP0454

```

DO 59 I=1,N
WRITE (6,146) (GKS(I,J,K), J=1,M)

```

MCSP0455
MCSP0456
MCSP0457

```

WRITE (6,150)

```

MCSP0458
MCSP0459
MCSP0460

```

DO 60 K=1, NSAM
WRITE (6,151) K

```

MCSP0461
MCSP0462
MCSP0463

```

DO 60 I=1,N
WRITE (6,146) (PKKS(I,J,K), J=1,N)

```

MCSP0464
MCSP0465
MCSP0466

```

61 WRITE (6,156)
WRITE (6,152)
WRITE (6,153)

```

MCSP0467
MCSP0468
MCSP0469

```

DO 62 K=1, NSAM
WRITE (6,155)

```

MCSP0470
MCSP0471
MCSP0472

```

DO 62 I=1,N
WRITE (6,154) K,I,XM(1,I,K),ERR(1,I,K),VAR(1,I,K)

```

MCSP0473
MCSP0474
MCSP0475

```

WRITE (6,156)

```

CH200082
MCSP0477
MCSP0478

```

146 WRITE (6,156)
147 FCRMAT (9(2X,IPE12.5),/)
148 FCRMAT (1,20X,OUTPUT DATA,///)
149 FCRMAT (10X,THE GAIN MATRICES ARE,/)
150 FCRMAT (5X,K=1,10X,G(K)=,/)
151 FCRMAT (1X,/,10X,THE THEORETICAL COVARIANCE MATRIX IS,/)
152 FCRMAT (5X,K=1,10X,P(K/K)=,/)
153 1 T51,SAMPLE MEAN OF,T16,VECTOR COM-,T34,SAMPLE MEAN,
153 1 FCRMAT (15,INDEX,T16,PONENT INDEX,T34,CF TRACK,
153 1 T51,ESTIMATION ERROR,T71,ESTIMATION ERROR)

```

MCSP0635
MCSP0636
MCSP0637
MCSP0638
MCSP0639
MCSP0640
MCSP0641
MCSP0642
MCSP0643

MCSP0644
MCSP0645
MCSP0646
MCSP0647
MCSP0648

```
154 FORMAT (6X,I3,I3X,I1,10X,1PE14.7,2(6X,1PE14.7))
155 FORMAT (//)
156 FORMAT (.1,)
157 FCRMAT (10X, THE SAMPLE COVARIANCE OF EST. ERROR MATRIX IS',//)
158 FORMAT (//,2X,'K=',I3,/)
      RETURN
      END
```

```
      SUBROUTINE PLT
      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),PHI(4,4),
      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
      3GAMMAS(4,4,60),PHIS(4,4,60),XS(4,4,60),HS(4,4,60),SIGW(4,4),
      4SIGXZ(4,4),XZMEAN(4,4),XHKK(4,4),VIMP(4,4),Z(4,4),X(4,4),
      5XHATZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),SIGV(4,4),
      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND,NR
      INTEGER*4 ITB(12)/12*0/
      REAL*4 RTB(28)/28*0.0/
      DIMENSION XP(60),YP(60)
      EQUIVALENCE (ITITLE,RTB(5))
      REAL*8 ITITLE(12),X = TRUE, + = FILTER, SQUARE = NOISY, /
```

C

```
      IGPLT=1
      ITHVPL=1
      INTPLT=1
      ISMPLT=1
      ISVPLT=1
      DO 500 KY=1,NR
      KX=NR+1-KY
      DO 50 K=1,NSAM
      XP(K) = XM(KX,1,K)
      YP(K) = XM(KX,3,K)
      CALL PLOTP(XP,YP,NSAM,0)
      CCNT INUE
      ITB(1)=1
      ITB(2)=1
      CALL DRAWP(60,XP,YP,ITB,RTB)
      DO 51 K=1,NSAM
      XP(K)=XS(1,1,K)+ERR(1,1,K)
      YP(K)=XS(1,3,K)+ERR(1,3,K)
      CALL PLOTP(XP,YP,NSAM,0)
      ITB(1)=2
      ITB(2)=2
      CALL DRAWP(60,XP,YP,ITB,RTB)
      ITB(2)=0
      DO 2 J=1,60,5
      IF (ABS(PKKS(1,1,J)-PKKS(3,3,J)).GT.0) GO TO 11
```

CH2*****
CH2*****
CH2*****
CH2*****
CH2*****

CH200088
CH200089


```

        PKKS(1,1,J)=PKKS(3,3,J)+0.000001
11      CONTINUE
        THE=0.5*ATAN(2.*PKKS(1,3,J)/(PKKS(1,1,J)-PKKS(3,3,J)))
        IF(ABS(THE).GT.0) GO TO 10
        THE=0.000001
10      CONTINUE
        SIG2X=(PKKS(1,1,J)+PKKS(3,3,J))/2.+PKKS(1,3,J)/SIN(2.*THE)
        SIG2Y=(PKKS(1,1,J)+PKKS(3,3,J))/2.-PKKS(1,3,J)/SIN(2.*THE)
        WRITE (6,146) THE,SIG2X,SIG2Y
146      FORMAT (9(2X,1PE12.5),/)
        SX=(SIG2X)**.5*20.
        SY=(SIG2Y)**.5*20.
        PT=3.14159265/12.
        CT=COS( THE )
        ST=SIN( THE )
        DO 1 I=1,25
        XI=I
        XP(I)=SX*COS(PT*XI)*CT-SY*SIN(PT*XI)*ST+XS(1,1,J)
        YP(I)=SX*COS(PT*XI)*ST+SY*SIN(PT*XI)*CT+XS(1,3,J)
1      CALL DRAMP(25,XP,YP,ITB,RTB)
        DO 201 J=2,NR
        DO 200 K=1,NSAM
        XP(K)=XS(J,1,K)
        YP(K)=XS(J,3,K)
200      IT=(J/2)+3
        ITB(2)=IT
        CALL DRAMP (60,XP,YP,ITB,RTB)
201      ITB(1)=3
        ITB(2)=3
        CALL DRAMP(60,XZ,YZ,ITB,RTB)
        DO 65 K=1,NSAM
        XP(K) = K
        C
65      IF (IGPLT.NE.1) GO TO 68
        C
        DO 67 I=1,N
        C
        DO 67 J=1,M
        C
        DO 66 K=1,NSAM
        YP(K) = GKS(I,J,K)
        C
66      WRITE (6,156)
        CALL PLOTIP (XP,YP,NSAM,0)
        C
67      WRITE (6,159) I,J
        C
68      IF (ITHVPL.NE.1) GO TO 71
        C

```

CH200090
CH200091

CH200092
CH200093
CH200094
CH200095
CH200096
CH200097
CH200098

MCSP0491
MCSP0492
MCSP0493
MCSP0494
MCSP0495
MCSP0496
MCSP0497
MCSP0498
MCSP0499
MCSP0500
MCSP0501
MCSP0502
MCSP0503
MCSP0504
MCSP0505
MCSP0506
MCSP0507
MCSP0508


```

C      DO 70 I=1,N
C      DO 69 K=1,NSAM
C      69 YP(K) = PKKS(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      70 WRITE (6,160) I,I
C      71 IF (IMTPLT.NE.1) GO TO 74
C      DO 73 I=1,N
C      DO 72 K=1,NSAM
C      72 YP(K) = XM(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      73 WRITE (6,161) I
C      74 IF (ISMPLT.NE.1) GO TO 77
C      DO 76 I=1,N
C      DO 75 K=1,NSAM
C      75 YP(K) = ERR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      76 WRITE (6,162) I,I
C      77 IF (ISVPLT.NE.1) GO TO 80
C      DO 79 I=1,N
C      DO 78 K=1,NSAM
C      78 YP(K) = VAR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      79 WRITE (6,163) I
C      80 CONTINUE
C      WRITE (6,156)
C      156 FORMAT (11)
C      159 FCFORMAT (12X,'G(',I1,',',I1,',',VS,K')'
C      160 FFORMAT (12X,'PKK(',I1,',',I1,',',VS,K')'
C      161 FFORMAT (12X,'MEAN OF X(',I1,',',I1,',',VS,K')'

```

```

MCSP0509
MCSP0510
MCSP0511
MCSP0512
MCSP0513
MCSP0514
MCSP0515
MCSP0516
MCSP0517
MCSP0518
MCSP0519
MCSP0520
MCSP0521
MCSP0522
CH200099
MCSP0524
MCSP0525
MCSP0526
MCSP0527
MCSP0528
MCSP0529
MCSP0530
MCSP0531
MCSP0532
MCSP0533
CH2
MCSP0535
MCSP0536
MCSP0537
MCSP0538
MCSP0539
MCSP0540
MCSP0541
MCSP0542
MCSP0543
MCSP0544
MCSP0545
MCSP0546
MCSP0547
MCSP0548
MCSP0549
MCSP0550
MCSP0551
MCSP0649
MCSP0650
MCSP0651

```



```

162 FORMAT (12X, 'XHATKK(', I1, ') -X(', I1, I1, ') VS. K.')
163 FORMAT (12X, 'ERROR VARIANCE(', I1, ') VS.. K.')

```

```

162 FORMAT (12X, 'XHATKK(', I1, ') -X(', I1, I1, ') VS. K.')
163 FORMAT (12X, 'ERROR VARIANCE(', I1, ') VS.. K.')

```

```

//GO.FT06F001 DD SYSOUT=A,SPACE=(CYL,(4,1))
//GO.SYSIN DD *

```

DATA DECK \$\$\$\$\$\$

NR	4
NENS	1
NSAM	60
IN	2
M	1
N	4

ND	IPRT	IPLT	PHI
4	1		
1.0		1.0	1.0

H
1.0
1.0
1.0

1.0 R
0.0001 COW
.0001
-0.0001

0.5
1.0
PKX M1

.0001	1000
.0001	1000
.0001	1000
.0001	1000

.0001	PRR(1)	.0001
.0001	.0001	.0001
.0001		.0001
.0001		.0001

.0001	PRR (2)	.0001	.0001
.0001	.0001	.0001	.0001
	PRR (3)		.0001

10.
SIGV
1000.
1000.
1000.

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.0001 .0001

.0001

XHATZ - JET	10.
0.3333XHATZ - INFANTRY1	
XHATZ - INFANTRY2	10.
XHATZ - HELICOPTER	
-.055555XS - JET	10.
0.3333XS - INFANTRY1	
XS - INFANTRY2	10.
XS - HELICOPTER	
-.055555	

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-0.00166667

0.00166667
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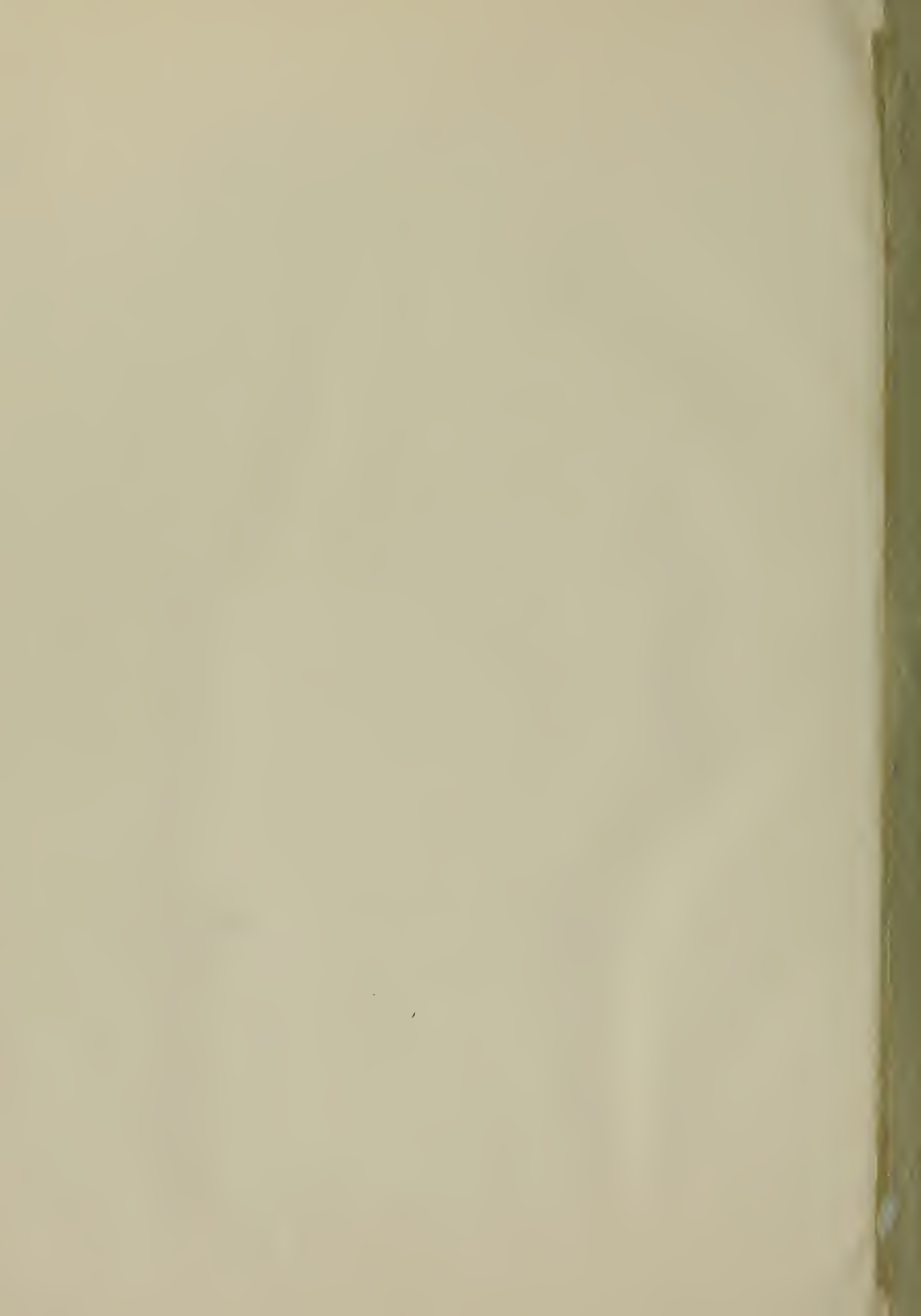
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